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AWS TECHNICAL REPORT
NO. 105-69

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HEADQUARTERS
AIR WEATHER SERVICE
ANDREWS AIR FORCE BASE
Washington 25, D. C.
27 April 1951

THEORY AND DESIGN
of a
GRADIENT WIND SCALE

1. Air Weather Service Technical Report No. 105-69, subject as above, will be changed as indicated in paragraph 2, effective upon receipt.

2. The following pen and ink changes will be made in Table A:

a. Page 12 -

Change the value "120" for $V_k = 20$, $V_g = 200$ to read "128."
Change the value "92" for $V_k = 80$, $V_g = 280$ to read "100."

b. Page 13 -

Delete the last line ($V_g = 160$, $G = 261$).

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AIR WEATHER SERVICE
TECHNICAL REPORT 105-69

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THEORY AND DESIGN
of a
GRADIENT WIND SCALE

November 1950

HEADQUARTERS
AIR WEATHER SERVICE
Washington, D. C.

HEADQUARTERS
AIR WEATHER SERVICE
Andrews Air Force Base
Washington 25, D. C.

November 1950

Air Weather Service Technical Report 105-69, "Theory and Design of a Gradient Wind Scale," is published for the information and guidance of all concerned.

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PREFACE

Numerous gradient-wind scales have been developed and reported upon in the literature. Although the principle of these scales may be applied to any map projection or scale, a different working model must be made in each case, and most of them are cumbersome to use.

The increased emphasis being placed on upper-wind analysis and forecasting necessitated the development of a simple yet accurate scale with universal applicability to all maps used by Air Weather Service.

Major Arthur F. Gustafson, of Headquarters, AWS, has developed such a scale and reports its design and use herein. The Weather Central at HQ, AWS, after trying various scales and tables for computing gradient-winds, found the one described here to be the most convenient.

THEORY AND DESIGN
OF A
GRADIENT WIND SCALE

Because of its wide scope of operations, the AWS must use various base maps with a wide diversity of scales and projections. For each different scale or projection, the appropriate geostrophic wind scale is different. Geostrophic wind scales for three or five mb isobar intervals are currently printed on most AWS base plotting charts. At many stations geostrophic wind scales for a 200-foot constant-pressure contour interval are already in use. It is anticipated that appropriate wind scales for use on constant pressure analysis will also be printed on the base charts. In any event, the theory underlying their design can be found in a paper by L. P. Harrison.^{1/}

By utilizing available (or easily constructed) geostrophic wind scales, a new gradient wind scale has been developed which is practically independent of the map scale and projection and therefore applies universally to all maps. The scale consists simply of a series of properly spaced arcs and is easily constructed. Used together with an appropriate geostrophic wind scale and a set of tables, this scale will give the gradient wind speed conveniently and accurately for all of the map projections used in the AWS. The simple theory underlying the design and use of such a scale is described below. The necessary tables are included at the end of this report.

^{1/} Harrison, L. P., 1948: Fundamental Relationships Involving Fields of Pressure and Geopotential. (April) pp. 22-31.

The gradient wind equation can be written

$$(1) \frac{1}{R} U^2 + g = f v - \frac{\Delta z}{\Delta n}$$

where: R is the radius of curvature of the "horizontal" trajectory (plus for cyclonic and minus for anticyclonic curvature).

$f = 2 \Omega \sin \Phi$ is the Coriolis parameter.

g is the acceleration of gravity.

v_g is the geostrophic wind.

Δz is the contour interval.

Δn is the spacing between adjacent contours.

Dividing equation (1) through by f we obtain

$$\frac{U^2}{f R} + \frac{g}{f} = v_g + \frac{\Delta z}{\Delta n}$$

If a curvature parameter V_1 is defined as

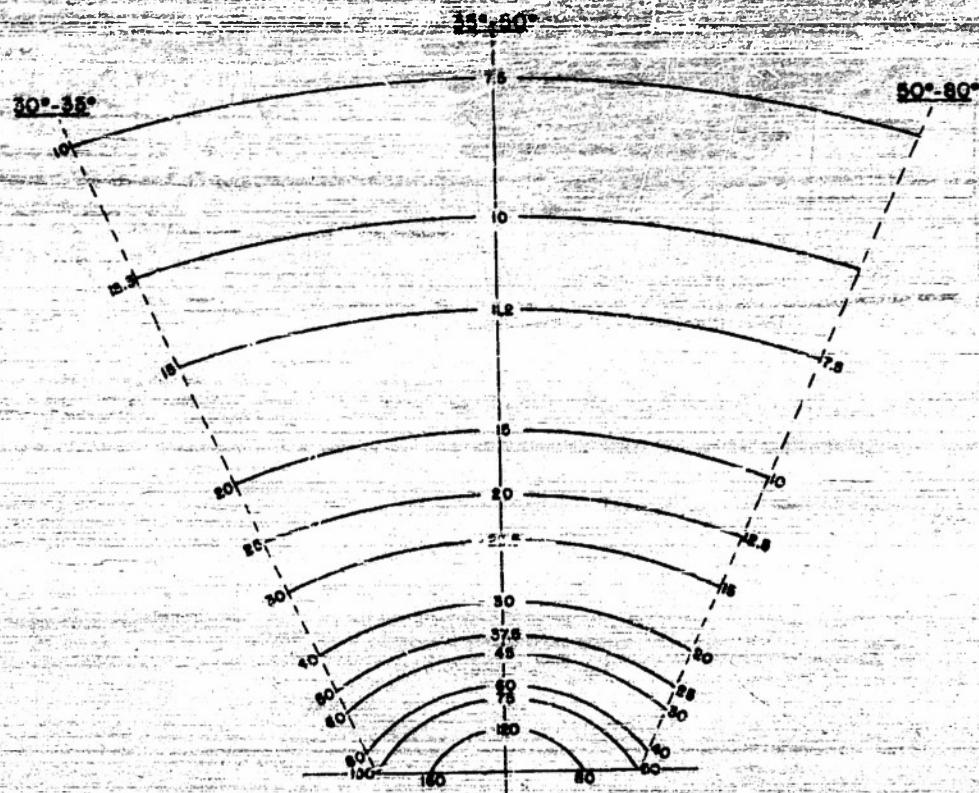
$V_1 = \frac{\Delta z}{f R}$ then equation (1) can be written

equation (1) can be written:

$$(3) \frac{1}{2 V_1^2} U^2 + g = v_g$$

Reference: "Introduction to Meteorology" by R. A. Ringer, McGraw-Hill, New York, 1945, pp. 175-80.

FIG 1



CURVATURE SCALE FOR
POLAR STEREOGRAPHIC (1.20×10^6 AT 60°)
N=2

0 1 2 3
OM

From equations (1) and (2) it can be seen that v_k' is defined in the same way as v_g except that Δn is replaced by R' . The curvature parameter v_k' can therefore be measured, using a geostrophic wind scale, by scaling off, along the proper latitude, a distance corresponding to R' in place of Δn . A "curvature scale", consisting of a series of circular arcs placed at distances from a reference point which are proportional to their radii, is used as an aid in making these measurements. An example of such a scale in which the arcs are placed at distances equivalent to one-half the radii of their corresponding circles, is shown in Figure 1.

The ratio (1:2) is most convenient for maps whose scale is $1:20 \times 10^6$ or thereabouts. For larger scale maps (e.g. $1:10^7$ or $1:12.5 \times 10^6$) a ratio (1:3) is preferable in order to avoid having too large distances representing significant radii of curvature. The speed v_k measured using these fractional parts of R' will of course be two or three times as great as the v_k' defined in equation (2). In fact, if $R' = R$ then $v_k = nv_k'$. Substituting this in equation (3), gives:

$$(4) \frac{v_k}{N g \Delta z_p} - G^2 + G = v \quad (N = 2, 3)$$

If v , G and v_k are in feet, and Δz_p is in feet, equation (4) becomes:

$$(5) \frac{v_k}{N g \Delta z_p} - 0.024 \cdot 0.001 v \quad \text{where } v \text{ is in feet}$$

Tables giving G as a function of V_x and V_y can be constructed from equation (5). Two sets of such tables, one (Table A) for $N\Delta p = 400$ (e.g. $N = 2$, $\Delta p = 200$) and another (Table C) for $N\Delta p = 600$, are included at the end of this report.

For use on surface charts with an isobar interval of Δp , the gradient wind equation corresponding to equation (4), is:

$$(4') \frac{V_x}{N\alpha_0 \Delta p} G^2 + G = V_g \quad (\text{where } \alpha_0 \text{ is the specific volume at sea level}).$$

For V_x , G and V_g in knots, Δp in millibars and $\alpha_0 = 800 \text{ m}^3/\text{ton}$, the equation corresponding to (5) is:

$$(5') \frac{V_x}{301.1 N \Delta p} G^2 + G = V_g$$

For $N = 3$ and $\Delta p = 5 \text{ mb}$, $301 N \Delta p = 4500$

but for $N\Delta p = 400$, $11.25 N\Delta p = 4500$

Table A may therefore be used for computing the gradient wind on surface charts provided the geostrophic scale is for a 5 mb interval and provided a $N = 3$ curvature scale is used. If the geostrophic wind scale is for 3 mb the same Table A can still be used provided the arguments V_x are relabeled as $3/5$ of their former values. For example, the column labeled $V_x = 25$ knots would be relabeled $V_x = 15$ knots. etc.

As mentioned previously, the exact value of V_g is found by scaling off the distance corresponding to R on the geostrophic wind scale at the proper latitude. Fortunately, however, the accuracy with

which V_k must be measured is not so critical as it is for V_g . The various arcs can therefore be labeled corresponding to their V_k values at two or three fixed latitudes, and these values can be used to a good approximation over a range of latitudes around them. The range of latitudes for which the values of V_k at a fixed latitude can be used depends on the type of map projection being used. If, for example, the map scale varied according to the sine of the latitude, the same contour spacing would everywhere represent the same geostrophic speed. For such a map, the range would be from 0° to 90° latitude. The polar stereographic projection, on the other hand, is an example in which the scale decreases with increasing latitude (and $\sin \phi$) so that the same map spacing of 1° represents even larger variations of the geostrophic wind with latitude than that due to the variations of the Coriolis parameter. On a 30° - 60° Lambert conformal projection, the scale increases with latitude above $45^\circ N$, and the variation of the geostrophic wind or V_k is therefore much smaller.

The curvature scale shown in Figure 1 is for a polar Stereographic map ($1:30 \times 10^6$ at $60^\circ N$) and has been labeled corresponding to its V_k values at approximately 32° , 41° , and at 60° . This choice gives a convenient (for labeling) 4:3:2 ratio of the respective V_k 's. The latitude ranges in which each set of these fixed latitude V_k 's can be used are 30° - 35° , 35° - 50° , and 50° - 60° respectively. For a Lambert conformal map only two fixed latitudes are necessary. Taking these as approximately

35° and 40° gives a convenient 4:3 ratio of the V_g 's and covers the latitudes ranges $30^{\circ}\text{--}45^{\circ}$ and $40^{\circ}\text{--}50^{\circ}$ respectively.

Now if the arcs are spaced according to their radii, the exact value of V_g can always be scaled off by placing the curvature scale on the geostrophic scale at the exact proper latitude. If this added accuracy is not desired, however, the arcs need not be spaced at distances proportional to their radii of curvatures. The spacing is then determined by convenience in labeling and by economy of space used. In this form the curvature scale may as well be put on the same piece of plexiglass as the geostrophic wind scale since it can no longer be used for exact scaling of V_g . An example of this form of the scale together with its corresponding geostrophic wind scale is shown in Figure 2.

In order to make the basic principles of the scale more easily understood, the discussion thus far has purposely avoided distinguishing between the actual curvature and the curvature of the trajectory.

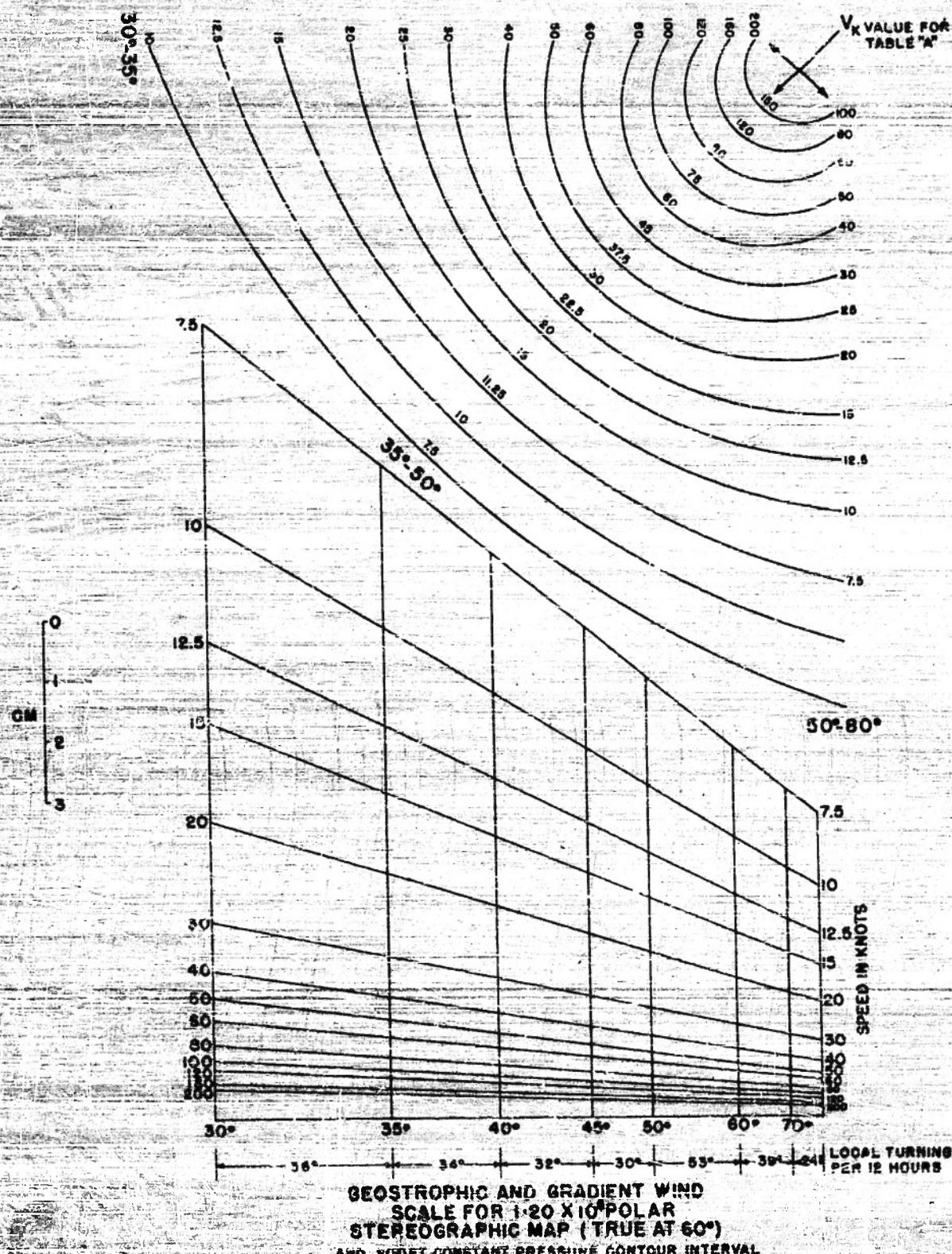
Obviously when an arc on the curvature scale is fitted to the contours, the contour curvature, not the trajectory curvature, is being measured.

In the following, however, it will be shown that this discrepancy can be taken care of by an adjustment in the latitude along which Δn and Δs are placed.

If the wind direction is assumed to be always the same as the geostrophic wind direction, the "horizontal" curvature of the trajectory will be related to the curvature of the contours K_g by the equation:

$$(6) \quad \bar{x} = K_g + \frac{1}{c} \frac{\partial v}{\partial t} \quad \text{or} \quad \frac{1}{R'} = \frac{1}{R_g} + \frac{1}{c} \frac{\partial v}{\partial t}$$

FIG 2



where $\frac{\partial \Psi}{\partial t}$ is the local time rate of turning of the geostrophic wind.^{4/}

Substituting this in equation (1) we have, on neglecting curvature,

$$\left(\frac{1}{R_g} + \frac{1}{G} \frac{\partial \Psi}{\partial t} \right) G^2 + CR = CV_g$$

or

$$(7) \quad \frac{1}{R_g} G^2 + \left(f + \frac{\partial \Psi}{\partial t} \right) G = CV_g$$

Comparing equations (1) and (7) it is seen that R_g may be used in place of R' , provided the latitude is adjusted in such a way as to account for the difference between f and $f + \frac{\partial \Psi}{\partial t}$. For cyclonic (counterclockwise) local turning an adjustment should be made such that smaller values of V_g and V'_g are obtained (usually toward higher latitudes) whereas for anticyclonic turning the adjustment should be made so as to give larger values of V_g and V'_g . The local turning in degrees per 12 hours, necessary to require an adjustment from one reference latitude to another (e.g. from 35° N to 40° N), are given below. These values, though independent of the map scale, are unfortunately not independent of

4/ The treatment here, as implied from the beginning by the use of the "horizontal" curvature, assumed either that the flow is horizontal or that the effects of the vertical motion can be neglected. The main effect neglected is that on the curvature of the trajectory due to a combination of vertical motion w and turning of the wind with height $\partial \Psi / \partial z$. The term $w/G (\partial \Psi / \partial z)$, which should be added to the right hand side of equation (6) due to this effect, can be as large or larger than the term $1/G \partial \Psi / \partial t$. Due to the difficulty in determining w , however, it is usually neglected.

the type of map projection.^{2/} Values are therefore given for the most common projections used in the ANS; i.e. the polar stereographic, the Lambert conformal 30°-60° N, and the Bonne's conformal 30°-75°.

Degrees per 12 hrs of Local Turning Corresponding
to Latitude Change $\phi_1 \leftrightarrow \phi_2$

(Values given are average of change from ϕ_1 to ϕ_2 and from ϕ_2 to ϕ_1)

$\phi_1 \leftrightarrow \phi_2$ Polar Stereographic - Lambert Conformal - Lambert Conformal
at various latitudes 30°-60° and 30°-75°

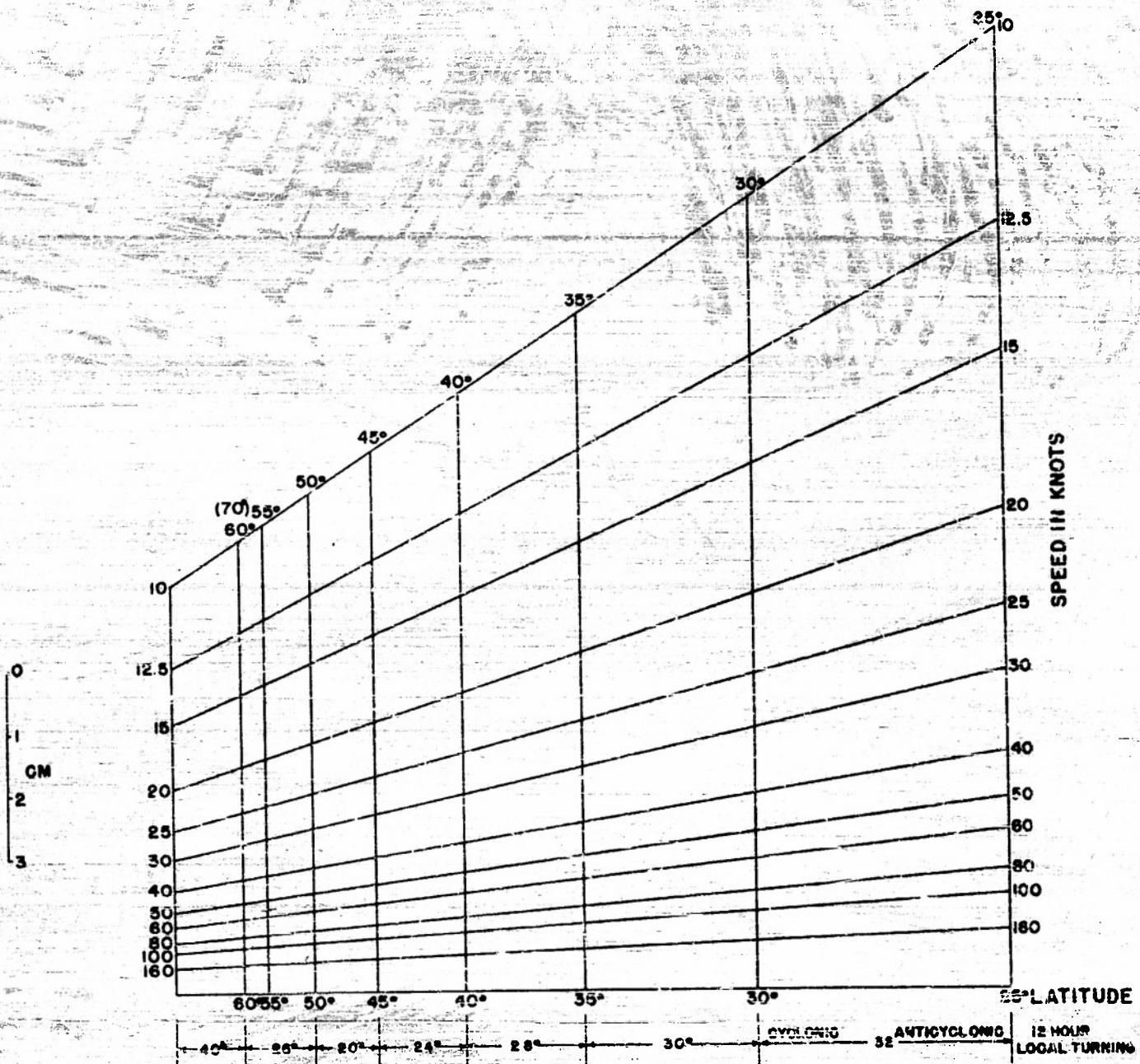
| | | | |
|---------|----|-----|-----|
| 25 - 30 | 27 | ±32 | ±34 |
| 30 - 35 | 36 | 30 | 32 |
| 35 - 40 | 34 | 28 | 30 |
| 40 - 45 | 32 | 24 | 27 |
| 45 - 50 | 30 | 20 | 24 |
| 50 - 55 | 28 | 16 | 20 |
| 55 - 60 | 25 | 10 | 16 |
| 60 - 65 | 29 | — | ±14 |
| 70 - 80 | 24 | — | — |

2/ It can be shown that the local turning ($\partial\psi/\partial\theta$)_{1/2} corresponding to a change in latitude from ϕ_1 to ϕ_2 is:

$$(\partial\psi/\partial\theta)_{1/2} = \frac{1}{\sqrt{\lambda}} \quad S_{\psi} = 360 \left(\sin \phi_1 - \frac{\phi_1}{\lambda} \sin \phi_2 \right)$$

where S_{ψ} is the scale variation as defined by L. P. Harrison (op cit).

FIG 3



GEOSTROPHIC WIND SCALE
FOR 200 FT CONTOUR INTERVAL ON 30°-60°
LAMBERT CONFORMAL $1:12.5 \times 10^6$

030951

In Figure 3 a geostrophic wind scale is shown for a Lambert conformal 30° - 60° map on which the approximate amounts of turning corresponding to an adjustment from one reference latitude to another have been entered.

The manner in which these values are used is illustrated by the following example. Suppose the point in question is at 33° and the local rate of turning has been estimated as 30° per 12 hours. On the Lambert conformal 30° - 60° map, 30 degrees of turning is seen to correspond to about a 5° adjustment of the latitude. The adjusted latitude is therefore taken as 38° . On the polar stereographic, on the other hand, the adjusted latitude would be $33^{\circ} + \frac{30}{36} \times 5^{\circ} = 37^{\circ}$.

Around 60° or 70° on the Lambert conformal 30° - 60° map, an adjustment may be required which cannot be identified with any latitude.^{6/}

A point representing 40° of cyclonic turning from 60° , however, can be located on the type of geostrophic wind scale shown in Figure 2, as follows: — Extend the 15 knot line from 60° until its Δn value is equal to the Δn^* for the 20 knot line at 45° . From this point draw a line parallel to the 60° N latitude line and then extend the remaining

$V_g = \text{const.}$ line as shown in Figure 2.

The local turning $\frac{d\theta}{dt}$ can be estimated in various ways. The past 12 hour turning of the contours, for example, may often be taken as an indication of the instantaneous rate of turning, provided that approximately the same rate of turning can be anticipated judging from a 12-hour prognosis.

^{6/} The same is true for a 30° - 75° Lambert conformal around 70° or 75° .

If the contour system is moving without appreciable change of shape, the local rate of turning can be estimated from the propagation of speed of the system and the curvature of the contours. Rather than do this and then adjust the latitude as described above, however, it is simpler to "correct" V_g by multiplying it by the ratio: $\frac{V_g}{V_g + V_p}$, where V_p is the geostrophic wind speed and V_g is the initial speed of propagation of the cyclone. This ratio is given by the formula:

$$\frac{V_g}{V_g + V_p} = \frac{1}{1 + \frac{V_p}{V_g}}$$

where V_g is a first estimate of the gradient wind and V_p is the zonal component of the propagation velocity in the direction of the geostrophic wind. When this "correction" is made, no adjustment is made in the latitude.

Although the gradient wind scale described above can be used anywhere on the map, it should be realized that the gradient wind speed is more representative of the true wind speed under certain circumstances than under others. Having been based on the assumption that the motion is frictionless, quasi horizontal and constant in speed, the gradient wind cannot be expected to give good results at low elevations over rough or mountainous terrain. For reasons mentioned above (see footnote 4), the gradient wind is also likely to be less reliable where the wind (or the geostrophic wind) veers or backs rapidly (e.g., 20° per 5,000 ft. or more) with height. It may also be stated both on theoretical and empirical grounds that the gradient wind speed is most applicable (as opposed to the geostrophic wind, for example) when the speed is high (e.g., > 50 knots) and when the curvature of the contours is cyclonic.

Fortunately when the geostrophic wind speed is weak, rawin, if not pibal or rabal observations, are more likely to be available since low elevation angles resulting in termination of SCR 658 rawin observations will not occur. Furthermore, in those situations where the curvature is anticyclonic (and the gradient wind is less reliable), the skies are more likely to be clear, permitting pibal or rabal observations. Under these conditions, weak winds or anticyclonic curvature (or both), observed wind speeds, if available, should be used to the fullest extent even though they differ from the computed gradient wind speed.

REFERENCES

- Harrison, L. P., 1946: Fundamental Relationships involving Field of Pressure and Geopotential. (April) pp. 32-31. SCR 658
- Willis, J. F., 1950: A Geostrophic Map. Bull. Am. Meteor. Society, November 1950.
- Holmboe, J., Forsythe, G. E., and Gustin, W., 1945: Dynamic Meteorology. pp. 178-80.

TABLE A

(N_A_p = 400)

Cyclonic

| | 7.5 | 10 | 12.5 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 | 120 | 160 |
|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|----|-----|-----|-----|
| 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | 9 | 9 | 9 | 8 | 8 | 8 |
| 15 | 15 | 14 | 14 | 14 | 14 | 14 | 14 | 12 | 12 | 13 | 13 | 12 | 13 | 11 |
| 20 | 19 | 19 | 19 | 19 | 18 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 14 | 14 |
| 25 | 24 | 24 | 22 | 22 | 21 | 21 | 22 | 21 | 20 | 20 | 19 | 18 | 17 | 16 |
| 30 | 29 | 28 | 26 | 26 | 27 | 26 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 18 |
| 35 | 33 | 33 | 32 | 32 | 31 | 30 | 29 | 28 | 27 | 26 | 24 | 23 | 22 | 20 |
| 40 | 38 | 37 | 36 | 36 | 35 | 34 | 33 | 31 | 30 | 29 | 27 | 26 | 24 | 22 |
| 45 | 42 | 41 | 40 | 40 | 38 | 37 | 36 | 34 | 33 | 32 | 29 | 28 | 26 | 24 |
| 50 | 46 | 45 | 44 | 44 | 43 | 41 | 40 | 37 | 35 | 34 | 32 | 30 | 28 | 26 |
| 60 | 55 | 54 | 53 | 51 | 49 | 48 | 46 | 43 | 41 | 39 | 36 | 34 | 32 | 29 |
| 70 | 63 | 63 | 60 | 59 | 56 | 54 | 52 | 49 | 46 | 44 | 41 | 38 | 35 | 33 |
| 80 | 72 | 69 | 67 | 66 | 64 | 62 | 58 | 54 | 51 | 49 | 45 | 42 | 39 | 36 |
| 90 | 80 | 77 | 75 | 73 | 70 | 65 | 63 | 59 | 56 | 53 | 48 | 45 | 42 | 38 |
| 100 | 87 | 84 | 82 | 79 | 75 | 72 | 69 | 64 | 60 | 57 | 53 | 48 | 45 | 41 |
| 110 | 95 | 91 | 88 | 86 | 81 | 77 | 74 | 68 | 64 | 61 | 58 | 51 | 48 | 43 |
| 120 | 104 | 98 | 95 | 92 | 87 | 82 | 79 | 75 | 68 | 64 | 58 | 54 | 51 | 45 |
| 130 | 117 | 113 | 108 | 104 | 98 | 93 | 88 | 81 | 76 | 72 | 65 | 60 | 53 | 48 |
| 140 | 131 | 126 | 120 | 116 | 108 | 102 | 97 | 89 | 83 | 79 | 71 | 65 | 61 | 55 |
| 150 | 145 | 135 | 122 | 127 | 118 | 111 | 105 | 97 | 90 | 85 | 76 | 70 | 62 | 56 |
| 160 | 158 | 150 | 143 | 157 | 129 | 120 | 114 | 104 | 97 | 91 | 82 | 75 | 70 | 63 |
| 170 | 164 | 173 | 155 | 157 | 146 | 136 | 129 | 117 | 109 | 102 | 91 | 84 | 78 | 62 |
| 180 | 206 | 195 | 185 | 176 | 163 | 153 | 143 | 130 | 120 | 112 | 92 | 92 | 86 | 76 |

TABLE A (Continued)

P. H. H. STANLEY

(from p. 124)

Anticyclonic

stability?

| | 12 | 14 | 16 | 18 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 | 120 | 160 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|-----|-----|
| | 12 | 14 | 16 | 18 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 | 120 | 160 |
| 0.1 | 12 | 14 | 16 | 18 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 | 120 | 160 |
| 0.2 | 15 | 16 | 16 | 16 | 16 | 17 | 17 | 18 | 19 | 21 | 21 | 21 | 21 | 21 |
| 0.3 | 21 | 21 | 21 | 22 | 22 | 22 | 24 | 26 | 28 | 31 | 31 | 31 | 31 | 31 |
| 0.4 | 25 | 26 | 27 | 27 | 28 | 29 | 30 | 32 | 37 | 41 | 41 | 41 | 41 | 41 |
| 0.5 | 30 | 32 | 32 | 33 | 34 | 35 | 38 | 41 | 45 | 51 | 51 | 51 | 51 | 51 |
| 0.6 | 35 | 37 | 38 | 39 | 40 | 43 | 46 | 48 | 53 | 58 | 58 | 58 | 58 | 58 |
| 0.7 | 40 | 43 | 45 | 46 | 48 | 50 | 53 | 56 | 61 | 66 | 66 | 66 | 66 | 66 |
| 0.8 | 45 | 48 | 51 | 53 | 55 | 58 | 60 | 63 | 68 | 73 | 73 | 73 | 73 | 73 |
| 0.9 | 50 | 53 | 56 | 59 | 60 | 63 | 66 | 69 | 74 | 79 | 79 | 79 | 79 | 79 |
| 1.0 | 55 | 58 | 61 | 64 | 65 | 68 | 71 | 74 | 79 | 84 | 84 | 84 | 84 | 84 |
| 1.1 | 60 | 63 | 66 | 69 | 70 | 73 | 76 | 79 | 84 | 89 | 89 | 89 | 89 | 89 |
| 1.2 | 65 | 68 | 71 | 74 | 75 | 78 | 81 | 84 | 89 | 94 | 94 | 94 | 94 | 94 |
| 1.3 | 70 | 73 | 76 | 79 | 80 | 83 | 86 | 89 | 94 | 99 | 99 | 99 | 99 | 99 |
| 1.4 | 75 | 78 | 81 | 84 | 85 | 88 | 91 | 94 | 99 | 104 | 104 | 104 | 104 | 104 |
| 1.5 | 80 | 83 | 86 | 89 | 90 | 93 | 96 | 99 | 104 | 109 | 109 | 109 | 109 | 109 |
| 1.6 | 85 | 88 | 91 | 94 | 95 | 98 | 101 | 104 | 109 | 114 | 114 | 114 | 114 | 114 |
| 1.7 | 90 | 93 | 96 | 99 | 100 | 103 | 106 | 109 | 114 | 119 | 119 | 119 | 119 | 119 |
| 1.8 | 95 | 98 | 101 | 104 | 105 | 108 | 111 | 114 | 119 | 124 | 124 | 124 | 124 | 124 |
| 1.9 | 100 | 103 | 106 | 109 | 110 | 113 | 116 | 119 | 124 | 129 | 129 | 129 | 129 | 129 |
| 2.0 | 105 | 108 | 111 | 114 | 115 | 118 | 121 | 124 | 129 | 134 | 134 | 134 | 134 | 134 |
| 2.1 | 110 | 113 | 116 | 119 | 120 | 123 | 126 | 129 | 134 | 139 | 139 | 139 | 139 | 139 |
| 2.2 | 115 | 118 | 121 | 124 | 125 | 128 | 131 | 134 | 139 | 144 | 144 | 144 | 144 | 144 |
| 2.3 | 120 | 123 | 126 | 129 | 130 | 133 | 136 | 139 | 144 | 149 | 149 | 149 | 149 | 149 |
| 2.4 | 125 | 128 | 131 | 134 | 135 | 138 | 141 | 144 | 149 | 154 | 154 | 154 | 154 | 154 |
| 2.5 | 130 | 133 | 136 | 139 | 140 | 143 | 146 | 149 | 154 | 159 | 159 | 159 | 159 | 159 |
| 2.6 | 135 | 138 | 141 | 144 | 145 | 148 | 151 | 154 | 159 | 164 | 164 | 164 | 164 | 164 |
| 2.7 | 140 | 143 | 146 | 149 | 150 | 153 | 156 | 159 | 164 | 169 | 169 | 169 | 169 | 169 |
| 2.8 | 145 | 148 | 151 | 154 | 155 | 158 | 161 | 164 | 169 | 174 | 174 | 174 | 174 | 174 |
| 2.9 | 150 | 153 | 156 | 159 | 160 | 163 | 166 | 169 | 174 | 179 | 179 | 179 | 179 | 179 |
| 3.0 | 155 | 158 | 161 | 164 | 165 | 168 | 171 | 174 | 179 | 184 | 184 | 184 | 184 | 184 |
| 3.1 | 160 | 163 | 166 | 169 | 170 | 173 | 176 | 179 | 184 | 189 | 189 | 189 | 189 | 189 |
| 3.2 | 165 | 168 | 171 | 174 | 175 | 178 | 181 | 184 | 189 | 194 | 194 | 194 | 194 | 194 |
| 3.3 | 170 | 173 | 176 | 179 | 180 | 183 | 186 | 189 | 194 | 199 | 199 | 199 | 199 | 199 |
| 3.4 | 175 | 178 | 181 | 184 | 185 | 188 | 191 | 194 | 199 | 204 | 204 | 204 | 204 | 204 |
| 3.5 | 180 | 183 | 186 | 189 | 190 | 193 | 196 | 199 | 204 | 209 | 209 | 209 | 209 | 209 |
| 3.6 | 185 | 188 | 191 | 194 | 195 | 198 | 201 | 204 | 209 | 214 | 214 | 214 | 214 | 214 |
| 3.7 | 190 | 193 | 196 | 199 | 200 | 203 | 206 | 209 | 214 | 219 | 219 | 219 | 219 | 219 |
| 3.8 | 195 | 198 | 201 | 204 | 205 | 208 | 211 | 214 | 219 | 224 | 224 | 224 | 224 | 224 |
| 3.9 | 200 | 203 | 206 | 209 | 210 | 213 | 216 | 219 | 224 | 229 | 229 | 229 | 229 | 229 |
| 4.0 | 205 | 208 | 211 | 214 | 215 | 218 | 221 | 224 | 229 | 234 | 234 | 234 | 234 | 234 |
| 4.1 | 210 | 213 | 216 | 219 | 220 | 223 | 226 | 229 | 234 | 239 | 239 | 239 | 239 | 239 |
| 4.2 | 215 | 218 | 221 | 224 | 225 | 228 | 231 | 234 | 239 | 244 | 244 | 244 | 244 | 244 |
| 4.3 | 220 | 223 | 226 | 229 | 230 | 233 | 236 | 239 | 244 | 249 | 249 | 249 | 249 | 249 |
| 4.4 | 225 | 228 | 231 | 234 | 235 | 238 | 241 | 244 | 249 | 254 | 254 | 254 | 254 | 254 |
| 4.5 | 230 | 233 | 236 | 239 | 240 | 243 | 246 | 249 | 254 | 259 | 259 | 259 | 259 | 259 |
| 4.6 | 235 | 238 | 241 | 244 | 245 | 248 | 251 | 254 | 259 | 264 | 264 | 264 | 264 | 264 |
| 4.7 | 240 | 243 | 246 | 249 | 250 | 253 | 256 | 259 | 264 | 269 | 269 | 269 | 269 | 269 |
| 4.8 | 245 | 248 | 251 | 254 | 255 | 258 | 261 | 264 | 269 | 274 | 274 | 274 | 274 | 274 |
| 4.9 | 250 | 253 | 256 | 259 | 260 | 263 | 266 | 269 | 274 | 279 | 279 | 279 | 279 | 279 |
| 5.0 | 255 | 258 | 261 | 264 | 265 | 268 | 271 | 274 | 279 | 284 | 284 | 284 | 284 | 284 |
| 5.1 | 260 | 263 | 266 | 269 | 270 | 273 | 276 | 279 | 284 | 289 | 289 | 289 | 289 | 289 |
| 5.2 | 265 | 268 | 271 | 274 | 275 | 278 | 281 | 284 | 289 | 294 | 294 | 294 | 294 | 294 |
| 5.3 | 270 | 273 | 276 | 279 | 280 | 283 | 286 | 289 | 294 | 299 | 299 | 299 | 299 | 299 |
| 5.4 | 275 | 278 | 281 | 284 | 285 | 288 | 291 | 294 | 299 | 304 | 304 | 304 | 304 | 304 |
| 5.5 | 280 | 283 | 286 | 289 | 290 | 293 | 296 | 299 | 304 | 309 | 309 | 309 | 309 | 309 |
| 5.6 | 285 | 288 | 291 | 294 | 295 | 298 | 301 | 304 | 309 | 314 | 314 | 314 | 314 | 314 |
| 5.7 | 290 | 293 | 296 | 299 | 300 | 303 | 306 | 309 | 314 | 319 | 319 | 319 | 319 | 319 |
| 5.8 | 295 | 298 | 301 | 304 | 305 | 308 | 311 | 314 | 319 | 324 | 324 | 324 | 324 | 324 |
| 5.9 | 300 | 303 | 306 | 309 | 310 | 313 | 316 | 319 | 324 | 329 | 329 | 329 | 329 | 329 |
| 6.0 | 305 | 308 | 311 | 314 | 315 | 318 | 321 | 324 | 329 | 334 | 334 | 334 | 334 | 334 |
| 6.1 | 310 | 313 | 316 | 319 | 320 | 323 | 326 | 329 | 334 | 339 | 339 | 339 | 339 | 339 |
| 6.2 | 315 | 318 | 321 | 324 | 325 | 328 | 331 | 334 | 339 | 344 | 344 | 344 | 344 | 344 |
| 6.3 | 320 | 323 | 326 | 329 | 330 | 333 | 336 | 339 | 344 | 349 | 349 | 349 | 349 | 349 |
| 6.4 | 325 | 328 | 331 | 334 | 335 | 338 | 341 | 344 | 349 | 354 | 354 | 354 | 354 | 354 |
| 6.5 | 330 | 333 | 336 | 339 | 340 | 343 | 346 | 349 | 354 | 359 | 359 | 359 | 359 | 359 |
| 6.6 | 335 | 338 | 341 | 344 | 345 | 348 | 351 | 354 | 359 | 364 | 364 | 364 | 364 | 364 |
| 6.7 | 340 | 343 | 346 | 349 | 350 | 353 | 356 | 359 | 364 | 369 | 369 | 369 | 369 | 369 |
| 6.8 | 345 | 348 | 351 | 354 | 355 | 358 | 361 | 364 | 369 | 374 | 374 | 374 | 374 | 374 |
| 6.9 | 350 | 353 | 356 | 359 | 360 | 363 | 366 | 369 | 374 | 379 | 379 | 379 | 379 | 379 |
| 7.0 | 355 | 358 | 361 | 364 | 365 | 368 | 371 | 374 | 379 | 384 | 384 | 384 | 384 | 384 |
| 7.1 | 360 | 363 | 366 | 369 | 370 | 373 | 376 | 379 | 384 | 389 | 389 | 389 | 389 | 389 |
| 7.2 | 365 | 368 | 371 | 374 | 375 | 378 | 381 | 384 | 389 | 394 | 394 | 394 | 394 | 394 |
| 7.3 | 370 | 373 | 376 | 379 | 380 | 383 | 386 | 389 | 394 | 399 | 399 | 399 | 399 | 399 |
| 7.4 | 375 | 378 | 381 | 384 | 385 | 388 | 391 | 394 | 399 | 404 | 404 | 404 | 404 | 404 |
| 7.5 | 380 | 383 | 386 | 389 | 390 | 393 | 396 | 399 | 404 | 409 | 409 | 409 | 409 | 409 |
| 7.6 | 385 | 388 | 391 | 394 | 395 | 398 | 401 | 404 | 409 | 414 | 414 | 414 | 414 | 414 |
| 7.7 | 390 | 393 | 396 | 399 | 400 | 403 | 406 | 409 | 414 | 419 | 419 | 419 | 419 | 419 |
| 7.8 | 395 | 398 | 401 | 404 | 405 | 408 | 411 | 414 | 419 | 424 | 424 | 424 | 424 | 424 |
| 7.9 | 400 | 403 | 406 | 409 | 410 | 413 | 416 | 419 | 424 | 429 | 429 | 429 | 429 | 429 |
| 8.0 | 405 | 408 | 411 | 414 | 415 | 418 | 421 | 424 | 429 | 434 | 434 | 434 | 434 | 434 |
| 8.1 | 410 | 413 | 416 | 419 | 420 | 423 | 426 | 429 | 434 | 439 | 439 | 439 | 439 | 439 |
| 8.2 | 415 | 418 | 421 | 424 | 425 | 428 | 431 | 434 | 439 | 444 | 444 | 444 | 444 | 444 |
| 8.3 | 420 | 423 | 426 | 429 | 430 | 433 | 436 | 439 | 444 | 449 | 449 | 449</ | | |

TABLE B

($\Delta z_p = 600$)

Cyclonic

| | 10 | 12.5 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 | 120 | 160 |
|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 5 | 58 | 76 | 81 | 87 | 97 | 104 | 114 | 124 | 134 | 144 | 154 | 164 | 174 |
| 10 | 10 | 10 | 10 | 20 | 20 | 30 | 30 | 39 | 39 | 49 | 49 | 49 | 49 |
| 15 | 15 | 15 | 14 | 14 | 24 | 34 | 34 | 34 | 34 | 43 | 43 | 43 | 43 |
| 20 | 19 | 19 | 19 | 19 | 19 | 38 | 38 | 38 | 38 | 47 | 47 | 47 | 47 |
| 25 | 24 | 24 | 24 | 28 | 38 | 48 | 48 | 48 | 48 | 58 | 58 | 58 | 58 |
| 30 | 29 | 28 | 38 | 28 | 27 | 37 | 37 | 38 | 38 | 48 | 48 | 48 | 48 |
| 35 | 33 | 33 | 33 | 32 | 31 | 51 | 50 | 50 | 50 | 58 | 57 | 55 | 54 |
| 40 | 38 | 37 | 37 | 35 | 36 | 35 | 33 | 33 | 33 | 31 | 30 | 28 | 27 |
| 45 | 42 | 42 | 41 | 40 | 39 | 38 | 37 | 36 | 34 | 33 | 31 | 29 | 27 |
| 50 | 47 | 46 | 45 | 44 | 43 | 42 | 40 | 39 | 37 | 35 | 33 | 32 | 29 |
| 55 | 51 | 50 | 49 | 48 | 47 | 46 | 44 | 43 | 40 | 38 | 36 | 34 | 31 |
| 60 | 55 | 54 | 54 | 52 | 50 | 49 | 47 | 45 | 43 | 41 | 38 | 36 | 33 |
| 70 | 64 | 63 | 62 | 59 | 58 | 56 | 53 | 51 | 49 | 45 | 43 | 41 | 37 |
| 80 | 72 | 71 | 69 | 67 | 65 | 63 | 59 | 57 | 54 | 50 | 47 | 45 | 41 |
| 90 | 80 | 79 | 77 | 74 | 73 | 69 | 65 | 62 | 59 | 55 | 51 | 48 | 44 |
| 100 | 88 | 86 | 84 | 81 | 78 | 75 | 70 | 67 | 64 | 59 | 55 | 52 | 47 |
| 110 | 96 | 94 | 91 | 87 | 84 | 81 | 76 | 73 | 68 | 63 | 59 | 55 | 50 |
| 120 | 104 | 101 | 95 | 94 | 90 | 87 | 81 | 77 | 73 | 67 | 62 | 58 | 53 |
| 140 | 118 | 115 | 112 | 105 | 102 | 98 | 91 | 86 | 81 | 74 | 69 | 65 | 59 |
| 160 | 134 | 129 | 125 | 118 | 115 | 108 | 100 | 94 | 89 | 81 | 76 | 71 | 64 |
| 180 | 148 | 142 | 138 | 130 | 124 | 118 | 109 | 102 | 97 | 88 | 82 | 76 | 69 |
| 200 | 161 | 158 | 150 | 141 | 134 | 128 | 118 | 110 | 104 | 94 | 87 | 82 | 73 |
| 240 | 185 | 180 | 175 | 162 | 153 | 146 | 124 | 125 | 117 | 106 | 98 | 91 | 82 |
| 280 | 213 | 203 | 198 | 182 | 171 | 163 | 148 | 138 | 130 | 117 | 108 | 100 | 90 |

TABLE B (Continued)

Anticyclonic

| $\frac{V_K}{V_G}$ | 10 | 13.5 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 | 120 | 160 |
|-------------------|-----|------|-----|-----|-----|----|----|----|----|----|-----|-----|-----|
| 10 | 10 | 10 | 10 | 10 | 10 | 10 | 11 | 11 | 11 | 12 | 12 | 13 | 16 |
| 15 | 15 | 15 | 15 | 16 | 16 | 16 | 17 | 17 | 18 | 19 | 22 | | |
| 20 | 21 | 21 | 21 | 21 | 22 | 22 | 23 | 24 | 26 | 32 | | | |
| 25 | 26 | 26 | 27 | 27 | 28 | 29 | 30 | 35 | 37 | | | | |
| 30 | 31 | 32 | 32 | 33 | 35 | 36 | 39 | 45 | | | | | |
| 35 | 37 | 38 | 38 | 40 | 41 | 43 | 50 | | | | | | |
| 40 | 43 | 43 | 44 | 46 | 49 | 53 | 65 | | | | | | |
| 45 | 49 | 50 | 51 | 53 | 57 | 62 | | | | | | | |
| 50 | 54 | 56 | 57 | 61 | 66 | 75 | | | | | | | |
| 55 | 60 | 62 | 64 | 69 | 77 | 95 | | | | | | | |
| 60 | 67 | 69 | 71 | 78 | 80 | | | | | | | | |
| 70 | 79 | 83 | 87 | 99 | 150 | | | | | | | | |
| 80 | 93 | 98 | 104 | 120 | | | | | | | | | |
| 90 | 107 | 114 | 124 | | | | | | | | | | |
| 100 | 122 | 133 | 150 | | | | | | | | | | |
| 110 | 138 | 154 | 191 | | | | | | | | | | |
| 120 | 157 | 180 | | | | | | | | | | | |
| 140 | 198 | | | | | | | | | | | | |
| 150 | 261 | | | | | | | | | | | | |

GRADIENT WIND G IN KNOTS

Formula: $\frac{V_K}{6,750} \cdot G^2 + G = V_G$

 V_G = geostrophic speed (knots) V_K = curvature parameter